

### Introduction to GD & T: Pages 2 thru 8

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# Engineering & Design: Geometric Dimensioning

## 1 Introduction

The concept of Geometric Dimensioning and Tolerancing (GD&T) was introduced by Stanley Parker from Scotland in the late 1930's. However it was not used to any degree until World War II (WW II) because until then the vast majority of products were made in-house. The designer could discuss with the manufacturing personnel (die designer, foundry foreman, machinist, and inspectors) what features were to be contacted to establish the so called "centerlines" that were used on the drawing to locate features such as holes and keyways. Also when two (2) or more features were shown coaxial or symmetrical around these "centerlines", the questions that needed to be answered by the designer was, "how concentric or symmetrical do these features have to be to each other?". During WW II companies had to "farm out" parts because of the quantities/schedules. This meant the new manufacturer had to interpret the drawing hence the "centerlines" were often established by contacting features that were not functional or important and features produced from these incorrect "centerlines" were not at the location required. The parts did not assemble and/or did not function properly hence had to be fixed or scrapped. GD&T was the solution to this major problem. GD&T provides a designer the tools to have clear, concise, and consistent instructions as to what is required. It eliminates ambiguities hence everyone that is involved with the part will not have to interpret the dimensioning.

## 2 What is GD&T?

It is compilation of symbols and rules that efficiently describe and control dimensioning & tolerancing for all drawings (castings, machined components, etc.). It is documented in ASME Y14.5M which has the symbols, rules, and simple examples. Also ASME Y14.8 has guidance for casting and forging drawings.

## 3 Why should GD&T be used?

- a. It is a simple and efficient method for describing the tolerancing mandated by the designer of the part.
- b. It eliminates ambiguities as to what Datum features are to be contacted to establish the Datum planes and/or Datum axis that are to be used for locating other features. All inspection will result in the same result - the dimension is within or out of tolerance. Fig. 5-1 illustrates a simple example of ambiguities associated with the "old" type drawing. Fig. 5-2 illustrates the same example with GD&T.
- c. It simplifies inspection because hard gages can often be utilized and inspection fixtures are often mandated which simplifies inspection for production quantities.
- d. It forces the designer to totally consider function, manufacturing process, and inspection methods. The result is larger tolerances that guarantee function, but reduce manufacturing & inspection costs. Also the "bonus" or extra tolerance for certain conditions can result in significant production cost savings. In addition the time to analyze whether a missed dimension is acceptable is dramatically reduced.

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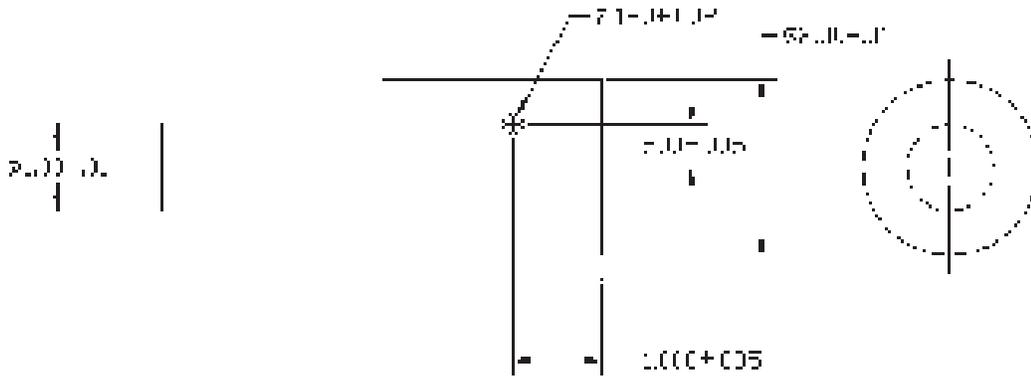


Fig. 5-1 "OLD" Drawing without GD&T.

## Questions:

- 1) What is the relationship (coaxiality tolerance) between the  $\varnothing 1.00$  and the  $\varnothing 2.00$ ?
- 2) Which feature ( $\varnothing 1.00$  or  $\varnothing 2.00$ ) is to be used for measuring (locating) the  $.500 \pm .005$  dimension for locating the  $\varnothing 1.20$  hole?

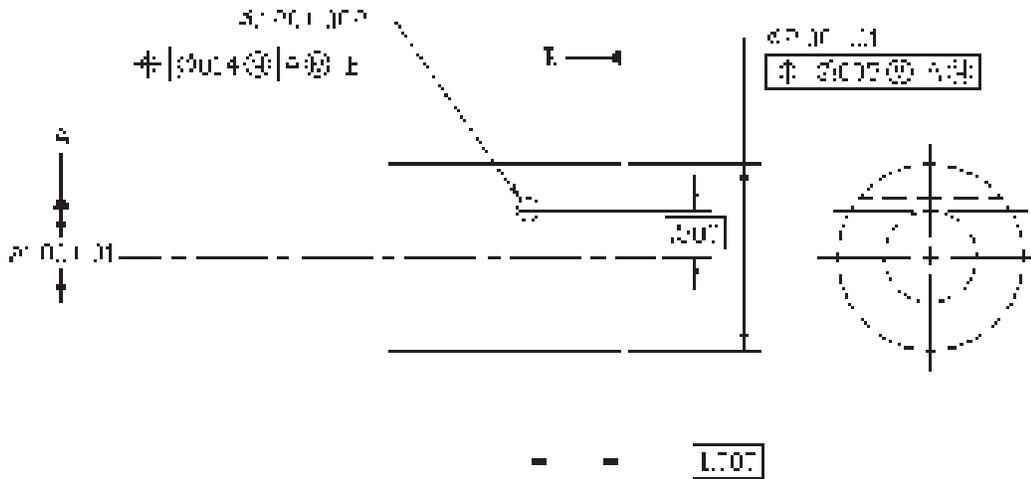


Fig. 5-2 "NEW" Drawing with GD&T.

## Questions asked in Fig. 5-1 answered:

- 1) The axis of the  $\varnothing 2.00$  has to be coaxial with the axis of the  $\varnothing 1.00$  within a tolerance zone that is a  $\varnothing .005$  if the  $\varnothing$  is 2.01 which is the MMC.
- 2) The  $\varnothing 1.00$  is the feature to be used for measuring the  $.500$  dimension for locating the  $\varnothing 1.20$  hole. The tolerance for locating the  $\varnothing 1.20$  hole is a  $\varnothing$  of  $.014$  (the diagonal of the rectangular tolerance zone shown in Fig. 5-1) when the hole is a MMC ( $\varnothing 1.20$ ).

## 4 Datum Reference Frame (DRF):

The DRF is probably the most important concept of GD&T. In order to manufacture and/or inspect a part to a drawing, the three (3) plane concept is necessary. Three (3) mutually perpendicular (exactly 90° to each other) and perfect planes need to be created to measure from. In GD&T this is called Datum Reference Frame whereas in mathematics it is the Cartesian coordinate system invented by Rene Descartes in France (1596-1650). Often one would express this concept as the need to establish the X,Y, and Z coordinates. The DRF is created by so-called Datum Simulators which are the manufacturing, processing, and inspection equipment such as surface plate, a collet, a three jaw chuck, a gage pin, etc. The DRF simulators provide the origin of dimensional relationships. They contact the features (named Datum Features) which of course are not perfect hence measurements from simulators (which are nearly perfect) provides accurate values and they stabilize the part so that when the manufacturer inspects the part and the customer inspects the part they both get the same answer. Also if the part is contacted during the initial manufacturing setup in the same manner as when it is inspected, a “layout” for assuring machining stock is not required. The final result (assuming the processing equipment is suitable for the tolerancing specified) will be positive.

### 4.1 Primary, Secondary, and Tertiary Features & Datums:

The primary is the first feature contacted (minimum contact at 3 points), the secondary feature is the second feature contacted (minimum contact at 2 points), and the tertiary is the third feature contacted (minimum contact at 1 point). Contacting the three (3) datum features simultaneously establishes the three (3) mutually perpendicular datum planes or the datum reference frame. If the part has a circular feature that is identified as the primary datum feature then as discussed later a datum axis is obtained which allows two (2) mutually perpendicular planes to intersect the axis which will be the primary and secondary datum planes. Another feature is needed (tertiary) to be contacted in order orientate (fix the two planes that intersect the datum axis) and to establish the datum reference frame. Datum features have to be specified in an order of precedence to properly position a part on the Datum Reference Frame. The desired order of precedence is obtained by entering the appropriate datum feature letter from left to right in the Feature Control Frame (FCF) (see Section 5 for explanation for FCF). The first letter is the primary datum, the second letter is the secondary datum, and the third letter is the tertiary datum. The letter identifies the datum feature that is to be contacted however the letter in the FCF is the datum plane or axis of the datum simulators. See Fig. 5-3 for Datum Features & Planes.

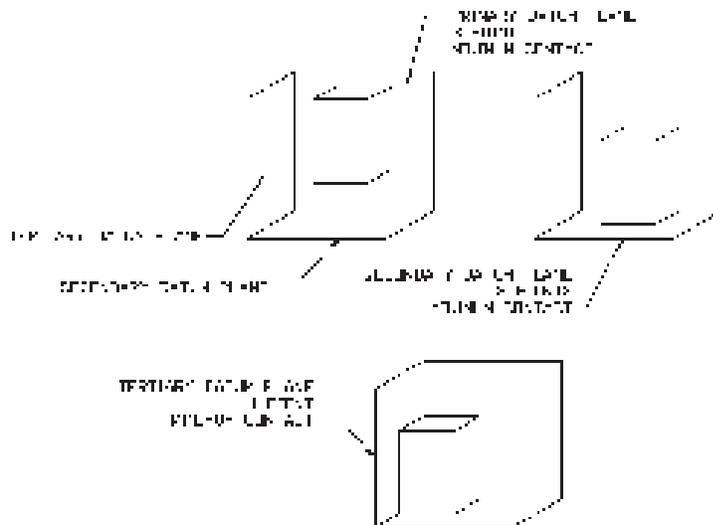


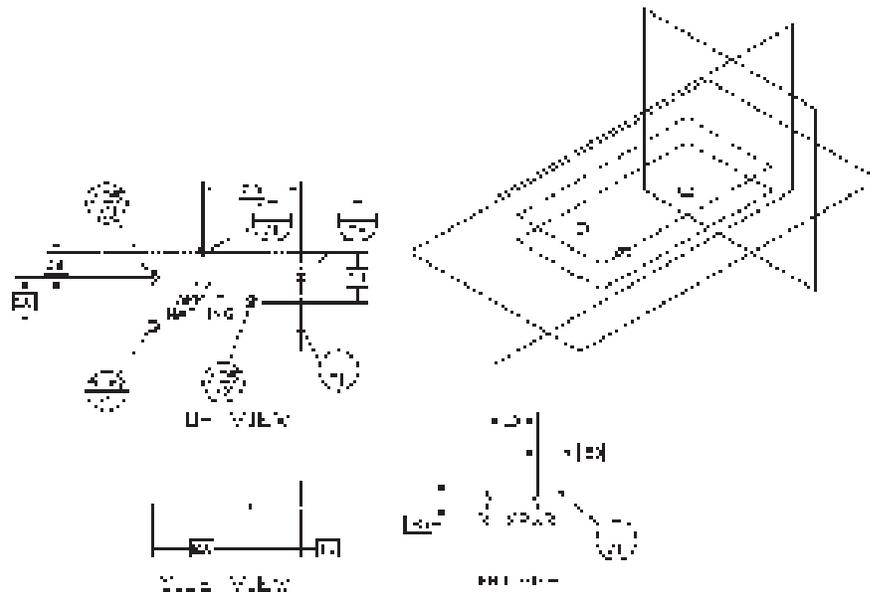
Fig. 5-3 Primary, secondary, tertiary features & datum planes.



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## 4.4 Datum Target Sizes & Locations:

Datum targets are datum simulators such as spherical pins or round flat bottom pins or three (3) jaw chucks or centers that establish datum planes or datum axis. They contact the datum features and are often specified to be used for inspecting parts that are inherently not round or straight or flat or they are large parts. If targets are not used then the entire datum feature has to contact a datum simulator. An example of what can result is the part could “rock” on a surface plate if the part was not relatively flat which would result in an unstable scenario and conflicting results. If the datum feature is large a datum simulator that contacts the entire feature may not exist or would be extremely expensive to produce. The datum targets are the datum planes and datum axis and often are assembled together to create an inspection fixture and or a manufacturing fixture. See Fig. 5-6 for Datum Target Sizes & Locations.



Component configuration shown as phantom lines on separate drawing

- Illustrates orientation when targets contact component
- Illustrates that targets are physically separate from the component
- Apply marking is shown to depict which side is to be contacted by the targets

Fig. 5-6 Target sizes & locations.

## 5 Feature Control Frame:

The geometric tolerance for an individual feature is specified in the Feature Control Frame which is divided into compartments - see Fig 5-7. The first compartment contains the type of geometric characteristic such as true position, profile, orientation, etc. The second compartment contains the tolerance (where applicable the tolerance is preceded by a diameter symbol and followed by a material condition symbol). The remaining compartments contain the datum planes or axis in the proper sequence (primary datum is the first letter).



Fig. 5-7 Feature control frame.

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## 6 Rule # 1 – Taylor Principle (Envelope Principle):

When only a size tolerance is specified for an individual feature of size the form of this feature shall not extend beyond a boundary (envelope) of perfect form at maximum material condition (MMC). In other words when the size is at MMC the feature has to be perfectly straight. If the actual size is less than the MMC the variation in form allowed is equal to the difference between the MMC and the actual size. The relationship between individual features is not controlled by size limits. Features shown perpendicular, coaxial or symmetrical to each other must be controlled for location or orientation otherwise the drawing is incomplete. In other words Fig. 5-1 is an incomplete drawing. Fig. 5-8 shows the meaning of Rule #1 for an external cylinder (pin or shaft) and an internal cylinder (hole). Note that a hard gage can be used to inspect this principle or requirement.

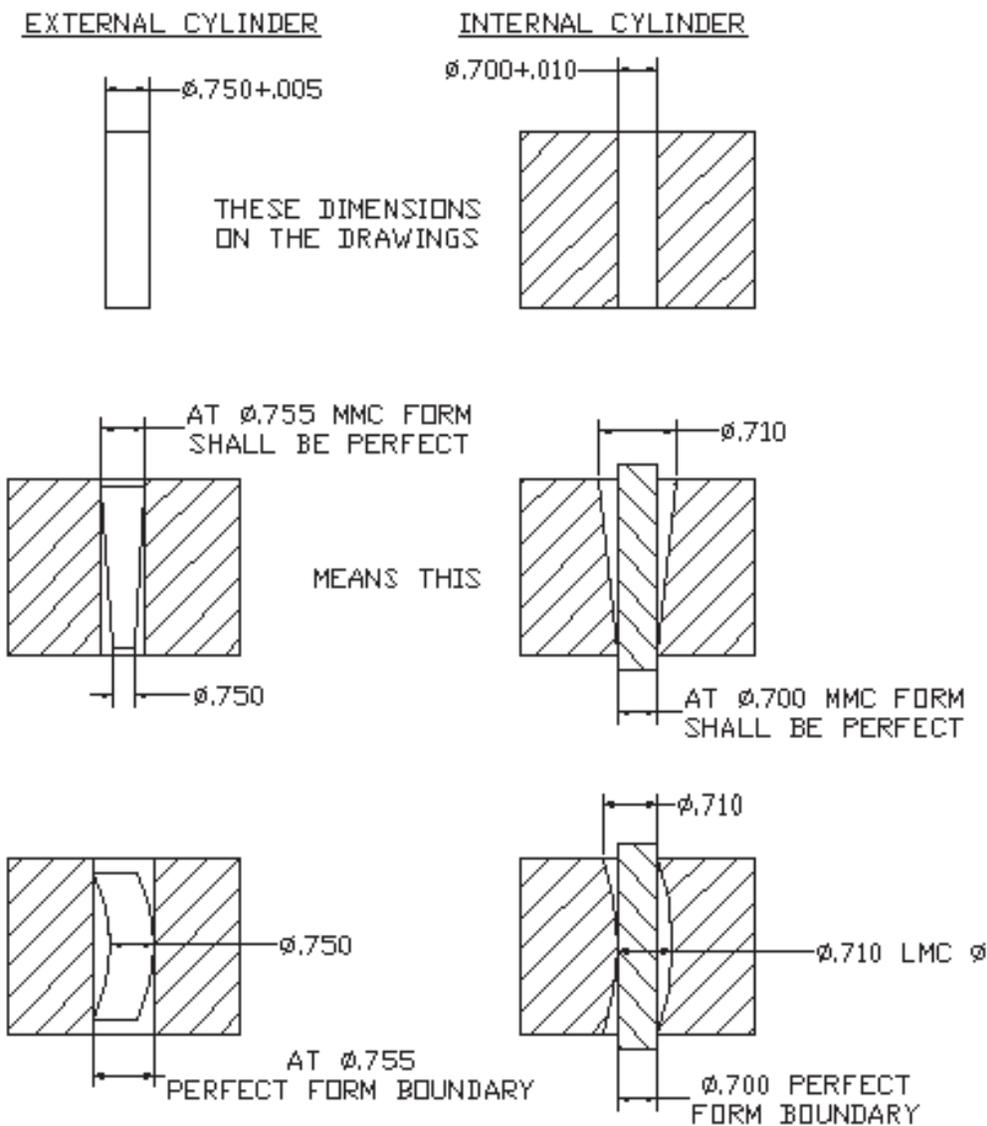


Fig. 5-8 Rule #1.

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## 7 GD&T Symbols / Meanings

Tolerance Type	Geometric Characteristics	Symbol	Applied To		Datum Reference Required	Use L or M Material Condition	Gages Used
			Feature Surface	Feature of Size Dim.			
Form	Straightness	—	YES	YES	NO	YES	YES***
	Flatness	▱		NO		NO	
	Circularity	○					
	Cylindricity	⊕					
Location	Positional Tolerance	⊥	NO	YES	YES	YES	YES***
	Concentricity	◎				NO	NO
	Symmetry	≡					
Orientation	Perpendicularity	⊥	YES	YES	YES	YES	YES***
	Parallelism	//					
	Angularity	∠					
Profile	Profile of a Surface	⌒	YES	NO	YES*	YES**	NO
	Profile of a Line	⌒					
Runout	Circular Runout	↗	YES	YES	YES	NO	NO
	Total Runout	↗↗					

\* Can be used to control form without a datum reference.

\*\* Datum reference only.

\*\*\* - Yes if M is specified for the feature of size being controlled

- No if S or L are specified for the feature of size being controlled.